



PEDOT:PSS-modified cotton conductive thread for mass manufacturing of textilebased electrical wearable sensors by computerized embroidery

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The textile industry has advanced processes that allow computerized manufacturing of garments at large volumes with precise visual patterns. The industry, however, is not able to mass fabricate clothes with seamlessly integrated wearable sensors, using its precise methods of fabrication (such as computerized embroidery). This is due to the lack of conductive threads compatible with standard manufacturing methods used in industry. In this work, we report a low-cost poly(3,4-ethylenediox vthiophene) polystyrene sulfonate (PEDOT:PSS)-modified cotton conductive thread (PECOTEX) that is compatible with computerized embroidery. The PECOTEX was produced using a crosslinking reaction between PEDOT:PSS and cotton thread using divinyl sulfone as the crosslinker. We extensively characterized and optimized our formulations to create a mechanically robust conductive thread that can be produced in large quantities in a roll-to-roll fashion. Using PECOTEX and a domestic computerized embroidery machine, we produced a series of wearable electrical sensors including a facemask for monitoring breathing, a t-shirt for monitoring heart activity and textile-based gas sensors for monitoring ammonia as technology demonstrators. PECOTEX has the potential to enable mass manufacturing of new classes of low-cost wearable sensors integrated into everyday clothes.

Respiration Monitoring; Gas Sensing

Introduction

Wearable sensors offer the possibility of monitoring health continuously using noninvasive devices attached to the body. This approach allows long-term monitoring of biophysical and (bio)chemical signals related to health and well-being, ranging from monitoring of activity, heart rate and breathing to levels of

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glucose, lactate or ions in sweat [1–4]. Continuous measurements provide an entirely new way to study the health of an individual by comparing them of today to themselves in the past [5]. This is particularly important for diagnosing diseases early and monitoring the effectiveness of treatments to improve outcomes. One of the main bottlenecks for emerging wearable sensors is that they often require the user to wear and carry around additional hardware that is needed for the measurements which can come in the form of watches, tattoos, patches and straps among others [6–10]. There is, of course, a practical limit to how many dedicated and standalone instruments one can wear on any given

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day; this limitation slows the adoption of many wearable innovations.

Textile fabrics are worn by everyone throughout the world as everyday clothes. Although clothes are in constant contact with the body, sensors are rarely incorporated into clothing in realworld applications. There are at least three big unaddressed challenges concerning the seamless integration of electrical and electrochemical sensors in clothing: materials and components used to produce sensors (*i*) alter the physical and chemical properties (*e.g.*, breathability, wettability, feel-on-the-skin) of fabrics; (*ii*) are generally not compatible with existing, well-established methods of fabrication used by the textile industry which predominantly rely on mechanically robust and durable threads/fibers and (*iii*) are vulnerable to cracking, delamination and chemical degradation during use or cleaning [11,12].

The textile industry has substantially computerized their manufacturing processes to increase the volume of production while reducing time and cost. To accelerate the adoption of new electrical sensing technologies by the textile industry, electrical sensing elements and interconnects must be compatible with the existing methods of manufacturing and should not require additional infrastructure or new high-cost instruments. Because mechanically robust organic fibers, yarns and threads, such as cotton, polyester and nylon, are the standard materials in the textile industry, there have been attempts to produce conducting or semiconducting versions of these materials through the application of organic and metallic coatings [13,14]. Yarns produced by coatings require complex synthesis and may use toxic compounds in the process [15–17]; most importantly, however, surface coatings applied are generally fragile and cannot withstand the mechanically harsh abrasive processes used in the manufacturing of textiles. Because of this, conductive organic yarns reported to date have either been exclusively hand embroidered to incorporate sensors into fabrics or required highly specialized and expensive instruments [18–20].

Computerized embroidery would allow the transfer of sensing structures with high spatial definition, designed on a computer, to fabrics in an accelerated fashion. The lack of conductive and semiconductive yarns compatible with computerized embroidery has particularly been a big issue to create sensors on fabrics reliably. Among all conducting polymers, the aqueous suspension of PEDOT:PSS has been used in textile coating applications and the construction of transducers on cotton-based substrates due to its processability and biocompatibility [21-23]. Müller and coworkers have reported computerized embroidery of all organic conductive silk yarns coated with PEDOT:PSS [24]. Their material exhibited high electrical conductivity (70 S cm^{-1}) before embroidery but upon embroidery, the conductivity of the yarns likely dropped significantly due to abrasion (note that the authors did not specify exactly how much this drop was). In another work by the same group, yarns of regenerated cellulose derived from wood pulp were coated with PEDOT:PSS, for some samples with Ag nanowires, and used in machine sewing of thermocouples for energy harvesting [25]. The authors used their yarn only in the bottom thread (or bobbin thread) configuration which sacrifices spatial definition for reduced tension and mechanical requirements for the thread. The bottom thread configuration is not commonly used for embroidering patterns by the textile industry due to poor appearance. Furthermore, the authors still relied on conductive silver paste added manually to connect thermocouples together to minimize resistive losses. Although Müller and coworkers have made progress toward all organic conductive threads, mechanical robustness and high costs of threads remain to be unsolved problems for fabricating sensors through computerized embroidery.

In this work, we report electrically conductive and mechanically robust all organic cotton-based low-cost threads that are fully compatible with domestic and industrial computerized embroidery machines. We solved the problem of mechanical robustness of conductive threads during embroidery by exploiting a crosslinking reaction using divinyl sulfone (DVS) as a crossroll-to-roll reaction involving poly(3,4linker in a ethylenedioxythiophene) polystyrene sulfonate (PEDOT:PSS), ethylene glycol (EG) and the cellulose substrate (Fig. 1). PEDOT:PSS-modified conductive cotton threads (PECOTEX) produced were structurally, mechanically, electrically/electrochemi cally characterized and used for the seamless integration of wearable electrical sensors into clothing. The novelty of this work is the modification of cotton threads with PEDOT:PSS using DVS to produce mechanically robust and machine embroidable lowcost conductive threads which can be used for high-volume production of wearable sensors using computerized embroidery. We produced facemasks for monitoring breathing, a t-shirt for monitoring heart activity and textile-based gas sensors for monitoring ammonia as technology demonstrators.

Results and discussion

Synthesis of PEDOT:PSS-based conductive threads

Before dying the cotton thread with the PEDOT:PSS-based conductive ink formulation, we pretreated the threads in an aqueous solution of a scouring detergent, METAPEX 38 (manufactured by ArtVanGo, UK) stirred at 80 °C for 2 h. We used a 3D-printed home-made desizing kit to allow internal magnetic stirring to improve penetration of the chemicals (Fig. S1) into thread. The detergent treatment was followed by oxidative desizing for 5 h using bleach (Waitrose, UK) to remove the cuticle layer which consists mostly of fats and waxes (see Supplementary Information Fig. S2 for more information on pretreatment). We chose oxidative desizing over other methods because it does not require a controlled environment for the removal of noncellulose byproducts. The threads were then rinsed several times in deionized (DI) water to clean the excess reagents and impurities. Pretreatment of the cotton thread is important to improve the adhesion of the conductive dye to the surface by increasing the number of reactive sites on the fibers which helps to produce a uniform and denser coating. After pretreatment, the cotton threads were dyed using a homemade, continuous roll-to-roll coating system (Fig. S2) which was digitally controlled by an Arduino microcontroller connected to a servomotor (Fig. 1a). This setup allowed passing a bobbin of thread through a sequence of vials containing liquid reagents/ink with adjustable speed. A standard blow-dryer (Red Hot Professional Hair Dryer) was used to blow hot air from a distance (~15 cm) to remove any excess water from the thread before winding on the bobbin to prevent sticking. With this setup, we were able to produce



(a) Schematic illustration of synthesis of the PEDOT:PSS-modified cotton thread (PECOTEX) and a photograph of the produced thread on bobbin. The inset shows the chemical structure of the product of the crosslinking reaction between PEDOT:PSS and cellulose surfaces within the cotton thread; (b) Process flow for the computerized embroidery of patterns using PECOTEX on cotton fabric (interdigitated electrodes) and 1 mm thick silicone (serpentine structures) substrates.

100 m of thread over a period of six hours in our laboratory in an automated fashion. The rate of production, however, could be increased by using squeeze rollers to control the amount of dye (PEDOT:PSS) deposited on the surface of the thread (Fig. S3). After dyeing the thread, it was left overnight at room temperature to allow the crosslinking reaction to take place before it was fed to the embroidery machine (Diamond Royale[™] by HUSQVARNA VIKING[®]). Embroidery designs were downloaded onto the computerized embroidery. After the substrate was placed in the hoop and inserted into the embroidery machine, the software design was embroidered on a substrate, lasting typically a few minutes.

Using the roll-to-roll coater, we produced six different types of threads (Fig. 2a) with different formulations, all of which included an aqueous dispersion of PEDOT:PSS as the conductive dye with reagents added to improve the electrical and physical characteristics of the final coating: (*i*) Type I thread was only coated with PEDOT:PSS. (*ii*) Type II included PEDOT:PSS + 5% wt. Dimethyl Sulfoxide (DMSO). (*iii*) Type III thread consisted of PEDOT:PSS + 5–10% wt. EG. (*iv*) Type IV contained PEDOT: PSS + 3–10% DVS. (*v*) Type V included PEDOT:PSS + 5% wt.

DMSO + 3% DVS. (vi) Type VI consisted of PEDOT:PSS + 3-7% wt. EG + 3-7% DVS. We chose DMSO and EG, widely studied cosolvents, as additives to improve the conductivity of PEDOT: PSS [26]. Since our eventual goal is to create mechanically robust conductive threads, that are compatible with computerized machine embroidery, to further improve the adhesion of PEDOT:PSS to the OH-rich surfaces of the cellulose fibers, we also experimented with the crosslinker DVS. Unlike other PEDOT:PSS crosslinking agents such as 3-glycidoxypropyltrimethoxysilane (GPTMS) [27] and 3-glycidyloxypropyl)trimethoxysilane (GOPS) [28], DVS increases the conductivity of crosslinked films. Furthermore, DVS has two vinyl reactive ends that can replace the hydrogen in OH groups, present on the cellulose surface and PSS by vinyl sulfone fragments via Oxa-Michael nucleophilic addition. DVS could, therefore, covalently crosslink different elements within the coating while also forming covalent bonds with the cellulose surface, similar to vinyl sulfone reactive dyes to textiles [29], to yield a robust conductive coating (Fig. 1a inset). Unreacted DVS acts as a second dopant to improve the conductivity of PEDOT, further increasing its utility as an additive [30].



FIGURE 2

(a) Electrical resistance of the conductive threads with different formulations before and after embroidery. Table provides a summary of all formulations. Error bars: SD, n = 5. (b) Raman spectra for planar films of the two most conductive formulations before and after embroidery (E5D3, 3D5). E3D5 was eventually selected because of smaller amount of dedoped PEDOT present in the film. (c). Normalized Raman spectra of E3D5 with and without pretreatment. Pretreatment increases –OH reaction sites on cellulose, hence the robustness of the coating.

Optimization of formulation of coating

To find the best formulation for a robust, PEDOT:PSS-based electrically conductive coating for cotton threads compatible with computerized embroidery and understand the role of each additive, we have performed a series of experiments. Because the most important characteristic for our threads is the electrical resistance (1/ electrical conductance), we measured the electrical resistance of each thread created with a different formulation before and after embroidery (Fig. 2a). The ideal thread for computerized embroidery should have the lowest electrical resistance before and after embroidery; to test the threads, a bobbin of the conductive thread was placed into the embroidery machine as top bobbin (Fig. S4) and square line stitches (stitch length 2 mm) of 25 cm² were embroidered onto a cotton textile using a domestic computerized embroidery system. We chose a square pattern because the abrasive forces exerted on the thread primarily originate in the eye of the needle and the magnitude of abrasion forces depends on the direction of embroidery. After embroidery, the embroidered patterns were unstitched, electrical resistance was measured using a multimeter and compared to before embroidery for each formulation (Fig. 2a). For all samples regardless of the formulation, the electrical resistance of the threads increased after embroidery due to the mechanical abrasion during stitching which breaks the conductive paths and par-

tially removes the coating (Video S1); however, while some formulations, such as Type I thread (i.e., coated with PEDOT:PSS only), exhibited a large starting resistance and a large increase in resistance after embroidery (electrical resistance before embroidery: 3.3 M Ω cm⁻¹, electrical resistance after embroidery: >40 M Ω cm⁻¹ – *i.e.*, beyond the limit of precision of the multimeter), Type VI thread - formulations consisting of PEDOT: PSS + 5% EG + 3% DVS (sample ID: E5D3) and PEDOT: PSS + 3% EG + 5% DVS (sample ID: E3D5) - had an electrical resistance of 800–1000 Ω cm⁻¹ before embroidery and 10–80 k Ω cm⁻¹ after embroidery. In these experiments, we have also noted that the addition of EG and DMSO also improved conductance of the threads before and after embroidery because of the uncoiling and stretching effect of the PEDOT chains which brings PEDOT molecules closer together facilitating the charge transport (Fig. S2). Different to DMSO, EG, however, is also known to increase the adhesion of PEDOT:PSS to hydroxyl (OH)-rich surfaces by hydrogen bonding [24]. Increasing the concentration of the EG enhanced the conductivity of thread before and after embroidery as the hygroscopic characteristics of EG also allows more water content to remain on the thread. The crosslinker DVS, when used on its own, performed better than PEDOT:PSS alone, but made the threads stiffer and more fragile especially at higher concentrations. Hence, a combination of PEDOT:PSS, EG and DVS performed the best due to enhanced hydrogen bonding and crosslinking between PEDOT:PSS, EG and the surface. The reaction of DVS with EG also produces a rubbery polymer as reported previously by Mantoine and coworkers [30] which improves the flexibility of the thread during embroidery hence produces a more mechanically durable coating.

In order to select the most optimum formulation between E5D3 and E3D5, we performed Raman spectroscopy for more detailed chemical and structural analysis of PEDOT, the conductive component in the coating (Fig. 2b and c). To eliminate the influence of the microstructure of the cellulose thread on the intensity of the signals, we first produced freestanding films in Petri dishes and performed the measurements (Fig. 2b). The experiments showed that E5D3 produced a stronger spectral intensity than E3D5 across the board. This result indicates that a larger amount of PEDOT in E5D3 is in resonance with the excitation wavelength hence, in a more dedoped (neutral) state than E3D5. This means that E5D3 is less conductive than E3D5, although the former showed lower measured electrical resistance than the later as in Fig. 2a. The difference in electrical resistance was associated with EG content, EG is hygroscopic by nature which means E5D3 contained temporarily more water molecules, hence was more conductive during the measurement. The addition of EG plays a significant role in increasing the conductivity through the conformational change of PEDOT chains from coiled to liner, but the excess of EG (>3wt % [31]) increases the distance between the isolated PEDOT molecules leading to reduced charge transport (Fig. S2). We, therefore, selected E3D5 for the rest of the experiments as the conductive coating for the cellulose thread.

We compared the normalized Raman intensities of E3D5 films coated on the cotton threads before and after embroidery and with and without pretreatment of the cellulose surface (Fig. 2c). The main features in this comparison are the relative intensity and broadening of the full width half maximum (FWHM) [32]. The spectra were normalized to C=C (located at 1425 cm⁻¹), so the relative intensity is the change in intensity of C–C intra peak (located at 1368 cm⁻¹). Without pretreatment of the cotton thread, the embroidery process had a significant effect on the PEDOT structure with a 24% increase in the relative intensity. This indicates a conformational change in the PEDOT structure as π electron density is shifted towards the intra-ring C-C bonds [33]. Additionally, there was a 4% broadening of the FWHM of the C=C peak. These changes indicate that there is a higher distribution of PEDOT conformations, hence a greater conformational disorder of the PEDOT segments was caused by the embroidery process. This suggests that PEDOT molecules were likely not anchored well on the surface of the fibers during coating which led to PEDOT structural changes during embroidery. In contrast, when the conductive coating was deposited on cotton threads with oxidative pretreatment, there was a lower degree of conformational change to the PEDOT segments after embroidery. The change in intra-ring C-C relative intensity was reduced to 7%, while the C=C peak FWHM was 1%. This observation agrees with the notion that pretreatment increases the number of -OH reaction sites on cellulose, therefore, improves the robustness of the coating during embroidery. Finally, we studied the impact of aging of E3D5 before and after embroidery by comparing normalized Raman spectra obtained after 24 h and seven days which remained unchanged over this period, indicating short-term stability (Fig. S5).

To further enhance the consistency of the coating, we coated the thread with four consecutive cycles of E3D5 formulation to produce PECOTEX. The electrical resistance of PECOTEX before embroidery improved to ~400 Ω cm⁻¹ after four cycles of coating. The electrical resistance after embroidery, however, did not change as most of the excess PEDOT:PSS coating was abrasively removed during embroidery.

Electro-mechanical and microstructural characterization of threads

In order to quantify the mechanical robustness of PECOTEX, we measured the tensile strength of threads that have been pretreated and coated with the conductive coating and compared the results to cotton threads (no coating) with and without pretreatment (Figs. 3a and S6). All threads tested could stretch approx. 20 mm and could withstand loads around 10 N. We noted, however, that the oxidative pretreatment process reduced the fracture strength of the threads up to 30%, likely due to the oxidative damage to the thread during pretreatment. The degree of damage could potentially be reduced by optimizing the pretreatment process. In any case, during embroidery, we did not observe snapping of the threads in our domestic computerized embroidery machine, suggesting that our coating process did not weaken the threads more than the loads experienced in a domestic embroidery machine to cause rapture. Using the force/displacement values shown in Fig. 3a (and by assuming a uniform diameter of 200 µm for the threads), we also estimated the stress-strain characteristics - please see Fig. S7 for more details.

We characterized the electrical properties of PECOTEX under cyclic tensile loading (Figs. 3b and S6). In this experiment, the



FIGURE 3

(a) Force-Displacement characteristics of the threads. Pretreatment weakens the thread, reducing its fracture strength, Error bars: SD, n = 5; (b) Change in resistance of PECOTEX under cyclic strain up to 10%; (c) Scanning electron and optical micrographs of a cotton thread, PECOTEX and PECOTEX after embroidery; (d) Machine washability test for embroidered PECOTEX patterns up to fifteen cycles, Error bars: SD, n = 5. The resistance remained largely unchanged over the experiment. (e) Cyclic voltammograms of PECOTEX with increasing scan rate and number of cycles of scans. The PECOTEX is stable and suitable for most electrochemical sensing applications.

threads were placed in a tensile tester and applied a periodically varying load between 2.5 N and 1.5 N with a frequency of 0.3 Hz for 1000 cycles. During this test the electrical resistance of the thread initially dropped likely due to the compression of the fibers together, increasing the number of parallel conductive paths within the thread. With repeated application of loading,

the resistance increased slowly as the conductive pathways were damaged due to cyclic strain. When the thread was released, its resistance increased ~40%, indicating the fibers that were compressed together were now released, disrupting the parallel conductive pathways and the damaged coating increased the overall resistance. We did not observe a cyclic change in the resis

tance of the threads with the application of cyclic loading, however. These results suggest that the conductive coating was robust enough to withstand cyclic loading without a large impact on its resistance. These results also suggest that these fibers are not suitable for reversible strain sensing applications but could be utilized as single use strain sensors.

To study the impact of embroidery and harsh mechanical conditions experienced by the threads, we have visually inspected the microstructure of PECOTEX before and after embroidery using scanning electron and optical microscopy (Fig. 3c). After the coating process, the diameter of PECOTEX decreased markedly in comparison to virgin cotton threads as the fibers were bound together by the excess coating (thickness = $3-9 \mu m$; Fig. S8) – the surface of the coated thread appeared smoother. The polymer coating also rendered the threads blue due to the intrinsic color of PEDOT. The diameter of the coated threads increased almost back to the same diameter as the original virgin cotton thread because of the mechanical forces applied during embroidery which removed some of the coating and unbound the fibers. The partial removal of the coating and structural damage after embroidery were also evident in the optical images of the thread which appeared to have a slightly lighter tone of blue; these observations agreed with the results of electrical characterization of the threads before and after embroidery (Fig. 2a) showing an increase in resistance after embroidery. Although there was a clear microstructural contrast between the PECOTEX before and after embroidery, the microstructure of PECOTEX after embroidery and virgin cotton thread was similar; PECOTEX could also be embroidered just as easily as the virgin thread – *i.e.*, the polymer coating did not render the cotton thread stickier and less machinable.

Because most clothes are machine washed and reusable, we also studied the machine washability of PECOTEX after embroidery (Fig. 3d) following the protocol described by the American Association of Textile Chemists & Colorists (AATTS) [18]. We machine embroidered $20 \times 2 \text{ mm}^2$ rectangular stitch patterns on a cotton textile substrate using the top-bobbin configuration and placed the patterns produced (n = 6) in a washing bag (Fig. S9). We measured the electrical resistance of the embroidered patterns (higher density samples) after five cycles of washing in a domestic washing machine (Candy GOW475 Washer Dryer). We dried the samples in an oven at 50 °C for 1 h between each wash cycle to remove all water from the samples before their electrical resistance was measured using a multimeter. After the 1st cycle of washing, the resistance of the embroidered patterns dropped ~50%, most probably due to the removal unreacted PSS from the coating which is a non-conducting molecule. In the subsequent cycles of washing, the electrical resistance of the embroidered patterns slowly increased until the 7th cycle and then remained stable thereafter, suggesting that PECOTEX is compatible with machine washing. The increase in electrical resistance until the 7th cycle can be attributed to mechanical removal of excess (unreacted) PEDOT:PSS from the surface of the cotton threads. Once the excess material was completely removed through washing, the electrical resistance remained stable up to 15 cycles. The small fluctuations observed are likely due slight random reconfiguration of the stitches during washing which

impact the conductance of the patterns embroidered. To study the impact of outdoor use of PECOTEX, we characterized the electrical stability of PECOTEX under different environmental conditions over a period of nine days. Elevated temperature (40 °C) had the largest impact on the electrical characteristics of PECOTEX, increasing its resistance, likely due to the partial degradation of PEDOT at elevated temperatures when exposed to air [34]. Exposure to solar irradiation, simulated rain or high relative humidity did not have a large impact (see supplementary information Fig. S10). We also characterized the long-term electrical stability of PECOTEX up to eight months (Fig. S11). We noted a slight increase in the electrical resistance of PECO-TEX, potentially due to the decrease of granular size of PEDOT with aging [34].

We have characterized the electrochemical properties of the PECOTEX since one of the application areas targeted with this technology is wearable electrochemical sensing. For that, a three-electrode electrochemical cell was constructed consisting of a 3 cm long PECOTEX as the working electrode (WE) which was attached to a commercial screen-printed electrode strip (DropSens, Metrohm) with a Ag/AgCl reference (RE) and C counter electrode (CE). In a solution of 20 mM ferrocyanide/0.1 M KCl, we first performed cyclic voltammetry (CV) at different scan rates (10, 20, 40, 60, 80, 100 mV s⁻¹) using ferrocyanide as an electrochemical probe (Figs. 3 and S12). We observed that the relation between the peak current (i_p) and the square root of the scan rate $(v^{1/2})$ was linear (Fig. S13) as expected for freely diffusing redox species according to Randles-Sevcik equation. This linear relationship indicates that the rate of electron transfer of species in solution is diffusion-limited and not limited by the material characteristics of the electrode [35]. This feature is important for the electrodes in electrochemical sensing in addition to high electrical conductance and chemical inertness. The peak-to-peak potential separation was observed to be higher than the ideal 59.2 mV, indicating a quasi-reversible oxidation/redox process [36]. The conducting polymer was sufficiently stable for 100 cycles (Fig. 3c) when measured at 100 mV s⁻¹, showing an increase in the peak currents after 20 cycles. This was probably due to the exposure of the probe to the evolving microstructure of the electrodes stabilized after continued cycling; PEDOT:PSS-based electrodes are known to change their microstructure when polarized in solution [37].

Fabrication of wearable sensors by computerized embroidery

To demonstrate the application of PECOTEX produced in this work, in wearable sensing, we have fabricated three different classes of proof-of-concept devices (Fig. 4) including: (*i*) a garment (in this case a t-shirt) with embroidered electrodes for measuring the electrical activity of the heart by electrocardiography (ECG); (*ii*) a disposable mask containing embroidered electrodes for monitoring respiration electrically and; (*iii*) embroidered gas sensors for sensing NH₃. After the fabrication of the sensors, we rinsed the embroidered patterns several times with DI water to remove unreacted DVS and EG, since they can cause skin irritation. The embroidered sensors retained the intrinsic properties of the fabric such as wearability, breathability and feel-on-the-skin.



(b) Respiration Sensor with Embroidered Electrodes





Sensor Mode I

Sensor Mode II

Gas Off

20



Gas On

(500 ppm)

10

Time (s)

15

100

80

60

0

5

Conductivity (a.u.)

Gas Off

Embroidered Sensor (Mode II) Response vs NH₃ Concentration



Continuous cardiac monitoring with an ECG t-shirt

Using computerized embroidery, we embroidered three electrodes (2.5×2.5 cm) on a textile t-shirt using PECOTEX for continuous monitoring of cardiac activity by ECG (Fig. 4a). ECG is an important tool routinely used in medicine for diagnosing and monitoring cardiovascular conditions but often requires continuous monitoring for extended periods of time, ranging from weeks to months [38]. We tested the ECG t-shirt for monitoring the electrical cardiac activity of a volunteer from our research group. After the volunteer put on the t-shirt, the embroidered electrodes were wetted with a conductive gel to improve the electrical contact with the skin - note that the gel penetrates the cotton t-shirt and electrodes providing excellent electrical contact (Video S2). We connected the embroidered electrodes to a microcontroller-based wireless ECG monitor and captured the cardiac activity of the volunteer while resting (Fig. S14). After digital signal processing (Figs. S15 and S16), the ECG waveforms captured by the embroidered electrodes were comparable to the waveforms captured by the commercial electrodes (Fig. 4a) in terms of noise artefacts. In both waveforms, the characteristic weaves such as the Q, R, S etc. were clearly identifiable allowing detecting of the heart rate and other important medical metrics, demonstrating that the ECG t-shirt could potentially be used for monitoring cardiac activity continuously. We also characterized the stability of our ECG and respiration sensors up to nine days (see supplementary information Fig. S17). We did not observe a noticeable difference in the quality of the signals generated by the sensor.

Electrical monitoring of respiration with an embroidered sensor

We have produced embroidered electrical respiration sensors on cotton textile substrates and embedded them in disposable facemasks (used commonly by the public during the COVID-19 pandemic) for continuous monitoring of respiratory activity (Fig. 4b). The respiration sensor consisted of two embroidered electrodes used for measuring the ionic conductance of the textile substrate; the ionic conductance originating from the dissociation of water adsorbed on the fibers of the textile to H₃O⁺ and OH⁻, changed during cycles of inhalation and exhalation which modified the level of moisture within the substrate [39]. The changes in moisture content (thus breathing) could be detected by applying an 5 V, 2 kHz AC signal between the electrodes and measuring the resulting ionic current running through the textile which is proportionally related to the ionic conductivity of the substrate. The signals originating from the sensors were transmitted using a cable connection between the

tom designed in our group, Figs. S18 and S19), we were able to capture respiratory activity from a volunteer and transmit the waveforms to a nearby mobile device running an Android app, developed also by our group (Video S3). With the embroidered respiration sensors, we could clearly detect different forms of respiratory activity including normal, paused, fast, shallow, slow and deep breathing without any post processing. By counting the peaks manually, the breathing rates (an important indicator of health and one of the four vital signs used in medicine [40]) for the different phases of respiratory activity could also be estimated. We compared PECOTEX-based embroidered textile respiration sensor to a commercial respiration sensor produced by Spyras Ltd. Both sensors produced comparable respiration waveforms (see supplementary information Fig. S20). We also characterized the stability of our respiration sensor up to nine days (see supplementary information Fig. S21). We did not observe a noticeable difference in the quality of the signals generated by the sensors.

sensor and electronics. Using portable wireless electronics (cus-

Embroidered gas sensors for sensing NH₃

For wearable sensing of gases, we produced embroidered gas sensors using cotton textiles as substrate (Fig. 4c). Because NH₃ has both diagnostic and environmental relevance, we tested the embroidered gas sensors for the detection of ammonia [41,42]. We produced two different types of chemiresistive gas sensors using PECOTEX with different underlying principles (or modes) of operation: Sensor Mode I consisted of a single continuous running stitch of PECOTEX and exploited the known phenomenon of dedoping of PEDOT when exposed to alkaline gases, which reduce the conductivity of PEDOT [43]. Sensor Mode II had a similar geometry to the respiration sensor described above, consisting of two embroidered electrodes of PECOTEX, separated by the textile substrate. Using this geometry, we measure the ionic conductivity of the hygroscopic, cellulose-based textile substrate, the conductivity of which changes when exposed to water soluble gases such as ammonia (this sensing approach was reported by our group previously – see [44] for more details).

Both Mode I Mode II sensors showed a response (that is change in conductivity G) when exposed to ammonia gas (Fig. 4c): expectedly, while the conductivity of Mode I sensors decreased when subjected to 500 part-per-million (ppm) of ammonia, the conductivity of the Mode II sensors increased. The conductivity of Mode I sensors did not recover back to their initial baseline, hence showed a cumulative response as gaseous NH₃ seemed to have modified the polymer permanently,

FIGURE 4

⁽a) Picture of a volunteer wearing a t-shirt with embroidered PECOTEX ECG electrodes for monitoring cardiac activity. PECOTEX and commercial ECG electrodes produce clear and comparable waveforms that contain all medically relevant information. The inset shows the side of the electrode in contact with the skin; (b) Picture of a volunteer wearing a disposable facemask containing embroidered PECOTEX electrodes for respiration sensing. The breathing patterns were captured using custom-made, battery-powered portable electronics and transmitted to a nearby mobile device for monitoring. Different respiratory activity was captured using the PECOTEX-based respiration sensor with low noise. (c) The electrical conductivity (normalized to 100%) of the PECOTEX-based embroidered gas sensors with two different sensing modalities when exposed to 500 ppm of ammonia at 70% relative humidity. The average change in electrical conductivity of the Mode II Sensor over a range of concentrations of NH₃ (5–1000 ppm) for n = 3 which shows an increasing response with concentration. The inset shows the response of PECOTEX-based embroidered Mode II Sensors (n = 3) when exposed to 200 ppm of NH₃ in two separate runs for the same sensors.

whereas Mode II sensors exhibited a semi-reversible response *i.e.*, when the flow of gas was shut-off, the conductivity of the sensor decreased but not completely back to the starting levels. We investigated the concentration dependent response of the Mode II sensors by exposing the sensors to varying levels of NH₃ up to 1000 ppm (Fig. S22). The sensors showed increasing response to higher concentrations in agreement with our previous work [44]; however, when we repeated exposing the sensors to the same concentration of gas, we noted that the sensor response decreased (Fig. 4c - inset). This is likely due to two competing processes of sensing of NH₃ using Mode II sensors: while the conductivity of the PECOTEX embroidered electrodes decrease when exposed to ammonia in a non-reversible fashion, the ionic conductivity of the textile substrate increased reversibly resulting in a semi-reversible gas sensor the performance of which likely will degrade with use over time. Both Mode I and Mode II sensors are, therefore, likely most suitable for shortterm use or will need to be regenerated by acid treatment after extended exposure to alkaline gases [45].

Conclusion

In conclusion, we have produced an all-organic cotton-based conductive thread (PECOTEX) that is compatible with domestic and industrial computerized embroidery machines. PECOTEX reported in this work can be produced at sufficiently low-cost using roll-to-roll processing (Table S1): the cost of materials was 0.15 USD m⁻¹ to produce low volumes of the conductive thread in our lab; we expect this number to decrease substantially when the production is scaled up industrially. PECOTEX exhibited superior characteristics compared to the commercially available Ag-based conductive threads including (Table S2): the average resistance after embroidery, number of breaks during embroidery, number of layers embroidered on top of each other etc. Furthermore, PECOTEX is compatible with computerized embroidery both in the top and bottom configuration as it can withstand the harsh mechanical conditions experienced during embroidery.

PECOTEX reported in this work have the following three disadvantages: (i) The electrical resistance of PECOTEX increase after embroidery up to 100 times. They remain, however, sufficiently conductive for most sensing applications [46-51]. Furthermore, the electrical resistance of the embroidered patterns can be reduced by denser stitching, using a longer stich length or deposition of additional materials by electroplating [48,52-54]. (ii) In comparison to metal-coated conductive threads, the electrical resistance of PECOTEX were a few orders magnitude higher; however, the electrical resistance of the metallic threads increased and became comparable to the PECOTEX after embroidery. (iii) Although we did not study in detail, we did notice a drop in electrical conductivity of the patterns embroidered with PECOTEX over time. Interestingly the electrical characteristics of the threads stored without embroidery remained stable over time.

Although in this work, we have only shown the application of PECOTEX for wearable monitoring of cardiac, respiratory activity and gas sensing, the material presented is suitable for a large range of other applications. These include, but not limited to, wearable electrochemical sensors [51,55,56], batteries [54], heaters [23], interconnects for wearable circuits and conductors for anti-electrostatic (ESD) clothing all of which can be produced at large volumes and cost-effectively through computerized embroidery.

Experimental methods

Pretreatment of cotton thread

Two-ply core-spun virgin cotton thread (JBS Olivia, South Korea) was desized by stirring in hot aqueous solution (80 °C) containing 5% wt. of Synthrapol (also known as METAPEX 38, from Kemtex), which consists of isopropanol and ethoxylated and sulfated aliphatic alcohols, for 2 h to remove water soluble and oily sizes. The thread then was immersed in a 4:1 (vol:vol) aqueous bleaching solution for 5 h. The solution contained sodium hydroxide (scouring agent) and sodium hypochlorite (oxidative desizing agent) to oxidize residual organic contaminants removing the "cuticle" (waxy layer) from the cotton fiber. The threads were washed several times with DI water before finally ovendrying at 50 °C for 1 h. The pretreatment efficiency was examined by applying water drops on the cotton thread. Successful pretreatment was confirmed with the formation of a hydrophilic

Roll-to-roll fabrication of the PECOTEX

thread.

We filled a 50 ml falcon tube with an aqueous solution of PEDOT:PSS (CLEVIOS PH 1000, produced by Heraeus), 3% wt of ethylene glycol (EG) and 5% wt of divinyl sulfone (DVS). EG and DVS were purchased from Sigma-Aldrich and used without any further modification. The cotton thread was first wound on a bobbin manually and pulled through four falcon tubes all containing the same PEDOT:PSS mixture (~5 ml each) using a servo-motor (Parallax Standard Servo) before winding on another bobbin after coating. The speed rotation of the servomotor was controlled by an Arduino Nano microcontroller board which was programmed using the Arduino IDE, installed on a Windows PC, over a USB connection. The optimum speed was found to be 3.6 m min^{-1} . After the thread was coated, before winding on the bobbin, it was briefly dried by a blow-drier to remove excess solvent to prevent sticking.

Computerized embroidery

Embroidery designs were made on a Windows PC using the PRE-MIER+TM 2 software. After the designs were completed, they were downloaded onto the computerized embroidery system (DESIGNER DIAMOND RoyaleTM by HUSQVARNA VIKING) before stitching. After the fabric substrate was placed in the hoop and inserted into the embroidery machine, the software design was embroidered on the substrate, lasting typically a few minutes. For embroidery on stretchable substrate, silicon (dragon skin 30) was cured in a 10 × 10 cm² mold (thickness 1 mm) for 5 h; then the substrate was removed from the mold and placed into the hoop with both sides covered with fabric supporting material (water soluble) to prevent sticking.

Raman spectroscopy

Resonant Raman spectroscopy was performed on the sample using a Renishaw inVia microscope in a back-scattering configu-

ration at an excitation wavelength of 633 nm with 10% of 12 mW laser power under $50 \times$ magnification. Samples were placed directly under the laser and focused to generate spectra. Multiple datasets of each sample were used to obtain an average representative spectrum for all normalized Raman spectra.

Microstructural characterization

Scanning electron micrographs were taken using JEOL, JSM-6010LA at 20 kV electron beam energy. The diameter of the virgin cotton thread was measured to be \sim 200 µm measured by electron microscopy (Fig. S23). The optical micrographs were obtained by a Brunel SP202XM metallurgical microscope. A Nikon D3200 camera was attached to the microscope for the acquisition of the images using DigiCamControl open-source software. For focus stacking to improve the limitation of depth-of-field, multiple images were taken at different focus and stacked together using Helicon Focus software.

Mechanical and electrical testing

The mechanical and electromechanical tests were carried out using a MultiTest 5-xt tensile testing machine controlled by Emperor Force software (Mecmesin) and 72-7730A source multimeter from TENMA. For mechanical testing, the thread samples were strained at a speed of 50 mm min⁻¹ until complete fracture. The (electro)mechanical tests were performed using PECOTEX samples of 10 cm in length. For electromechanical testing, PECOTEX samples were connected to the multimeter using crocodile clamps on both ends to measure their electrical resistance during the test. The PECOTEX samples were subjected to a cyclic force between 1 and 2.5 N. The electrical resistance of all samples was measured using the same multimeter as described above (*i.e.* 72-7730A from TENMA). The IV curves of PECOTEX were acquired using a Keithley 2450, Source-meter (Fig. S13).

Electrochemical testing

Cyclic voltammograms were acquired using a handheld potentiostat (PalmSens3, PalmSens BV, The Netherlands) with the supplied PSTrace 5.3 software in a three-electrode electrochemical cell configuration. A commercial screen-printed drop sensor (supplied from Metrohm DropSens, Switzerland) was used to conduct the measurements with 3 cm of PECOTEX attached to the strip as the working electrode, with printed Ag/AgCl as reference and C counter electrode. The scanning windows for the applied potential was set to -1.0 to 1.2 V with varying sweep rates. All electrochemical tests were performed in an aqueous solution of 0.1 M Potassium chloride (KCl from Sigma Aldrich) and 20 mM ferrocyanide (K₃[Fe(CN)₆] from Sigma Aldrich).

Washability experiments

The washability tests were conducted following the American Association of Textile Chemists & Colorists protocol by using a domestic laundry machine (Candy GOW475 Washer Dryer): The cotton fabrics embroidered with PECOTEX were placed into a washing bag and placed in the washing machine along with 1.8 kg of fabric serving as a ballast. The washing cycle lasted 60 mins in total: 50 mins of washing in water on handwashing mode and 10 mins of mechanical drying at 600 RPM and 30 °C. The electrical resistance measurements were taken

after drying the samples for 1 h at 50 $^{\circ}$ C in an oven in air. In order to confirm sufficient drying, one of the samples was left overnight before repeating measurements the next day which matched the initial readings (after 1 h at 50 $^{\circ}$ C).

ECG experiments

The ECG recordings were obtained from a volunteer using an ESP32-based microcontroller board attached to an AD8232 SparkFun Single Lead Heart Rate Monitor. The waveforms captured were transferred to a PC running MATLAB over WiFi. The waveforms collected were also post-processed in MATLAB (see supplementary information Figs. S15 and S16 for more information on post processing). The disposable commercial ECG pads were sourced from Amazon. The ECG cable was purchased from SparkFun. Conductive gel (Elektroden-Gel) was purchased from Amazon.

Respiration sensing experiment

For data acquisition, a custom-made read-out board based on ESP32 was used. An alternating voltage was applied across the sensing electrodes and an opamp (AD820)-based transimpedance amplifier was used to estimate the impedance of the sensors. The range of amplification was adjusted by switching between different gain resistors using a multiplexer (MAX335). The waveforms captured by the read-out board was transmitted to a nearby android phone in real-time via Bluetooth Low Energy (BLE) which contained a homemade app. See Figs. S18 and S19.

Ammonia sensing experiment

A homemade gas sensor characterization setup was used to adjust the concentration of ammonia in the sensing environment using three mass flow controllers (MFCs, type GM50A from MKS) while measuring the electrical conductance using a custom-board. For more information on the gas sensor characterization setup used see our previous publication [44].

All the human experiments were risk assessed.

Declaration of Competing Interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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Author contributions

F.A. performed all the experiments and collected and analyzed the data. He also did the writing, taking of pictures, recording and editing of videos, and making of animations. H-S.L. constructed the dyeing setup and assisted with collection of ECG and respiration data, he also assisted with recording of videos in the supporting information. G.B. constructed the ammonia detection setup and the electronics in the respiration experiments. G.B. developed the Android smartphone app and also performed the ammonia detection experiments and assisted with data analysis. E.T. performed the Raman measurements and analyzed the data. Y.C. assisted with the ECG experiment, postprocessing data and development of software. T.A. made and assisted with the animations. L.G-M. analyzed the electrochemical data. P.C assisted with taking of pictures and editing of videos in supplementary information. E.N-B. assisted with acquisition of electrochemical data and assembly electrochemical cell. J-S. K. assisted with Raman data analysis. F.G. supervised the research, edited the manuscript and figures and contributed to the videos.

Conflict of interest

F.G. is a non-operating co-founder of Spyras Ltd.

Data availability

The raw/processed data required to reproduce these findings cannot be shared at this time due to technical or time limitations.

Appendix A. Supplementary data

Supplementary data to this article can be found online at https://doi.org/10.1016/j.mattod.2022.07.015.

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